





Calculation of photoneutron contamination of Varian linac with new target in tissue equivalent phantom using Monte Carlo simulation

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Article Info	ABSTRACT
<p>Article type: Research Article</p> <p>Article history: Received: 30 Mar. 2022 Revised: 30 Apr. 2022 Accepted: 18 May. 2022 Published online: 14 Nov. 2022</p> <p>✉ Correspondence to: Dr. Tayyeb Pourfallah, Department of Medical Physics, Medical College, Pyambar Azam Academic Complex, Mazandaran University of Medical Sciences (MAZUMS), P.O. Box 48157-33971, Sari, Iran Tel: +98 11 33543256 Fax: +98 11 33352725 Email: tpourfallah@mazums.ac.ir</p>	<p>Introduction: In this research, a new material ($Ti_2V_{0.7}Cu_{97.3}$) was proposed for the target of medical linear accelerators (linacs) to reduce the production of unwanted photoneutrons in the radiotherapy. So, the fluence, dose equivalent and kerma of the photoneutrons were calculated in a soft tissue phantom.</p> <p>Materials and Methods: The medical linac was the Varian 2100 C/D 18 MV, which its tungsten target was replaced with a new multi-metal target ($Ti_2V_{0.7}Cu_{97.3}$). Desired quantities were computed in a ICRU soft tissue phantom, using the Monte Carlo code MCNPX (v. 2.6).</p> <p>Results: The ratio of the maximums of fluence, kerma, and dose equivalent of photoneutrons along the central axis of the ICRU phantom with new target rather than tungsten target were 72 %, 59 % and 61 %, respectively. Average of the Ratio of fluence, kerma, and dose equivalent in inner area (distances less than 5 cm from central axis) at different depths of the phantom with new target rather than tungsten target were 78 %, 70 % and 75 %, respectively. Uncertainties at all points were less than 5 % (except for a few points which were less than 10 %).</p> <p>Conclusion: This work showed that applying $Ti_2V_{0.7}Cu_{97.3}$ alloy for the target of linac, can reduce the produced photoneutrons up to 38 % by an applicable and inexpensive way.</p> <p>Keywords: MCNPX, Photoneutron contamination, Simulation, Target of linac</p>

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Introduction

Medical linear accelerators (linacs) are used for treating compact tumors extensively. Head of linacs mainly

constructed of heavy elements such as lead, tungsten, iron, copper and so on. When the applied energy is more than the threshold energy of (γ , n) or (e, n) reactions, (~ 8

MeV), some undesired photoneutrons and electroneutrons are produced which can deliver additional dose to patients, which possibly can cause secondary cancers after radiotherapy. Since quality factor of neutrons is about 2 - 20 times more than photons (i.e., varies with neutron energy) (1), they have a substantially higher biological effectiveness than photons. Therefore, even a small number of neutrons can lead to a non-negligible effective dose to patients, in the form of non-target and out-of-field dose (2).

Interactions between high energy treatment beam and nuclei of composing elements of the linac, beam collimation system, couch, patient's body, air and walls of treatment room can produce photoneutrons. Because the threshold energy of (γ , n) reaction for composing elements of the head of linac, such as lead, tungsten, copper and iron, is generally in the range of 6.74 - 11.20 MeV, interactions between high energy treatment beam and nuclei of composing elements of the medical linear accelerator (linac), couch, patient's body, air and walls of treatment room can produce photoneutrons (3).

Estimation of photoneutron contamination in radiotherapy (RT) has been studied by several researchers in various experimental and simulation methods (4-10). Bezak and his coworkers (11, 12) measured the total dose equivalent in Rando and water equivalent phantoms, using TLD and estimated the risk of secondary cancer in organs of Rando phantom in treatment of prostate. Sohrabi and Hakimi measured the dose of thermal and epithermal photoneutrons using a self-made experimental method within a polyethylene phantom (13). Bagheri et al. (14) and Bagheri et al. (15) measured the dose of thermal photoneutrons in treatment of breast cancer within the breast Rando phantom using TLD. Comparing the experimental results for photoneutron contamination show differences between results. It has been demonstrated that using the Monte Carlo code MCNPX, in

radiotherapy, can lead to reliable outputs and are accordance with experimental measurements. Barquero et al., (16) calculated the effects of total photoneutrons on various organs using MCNPX code in a computational phantom. Many others calculated the spectra of photoneutrons and dose equivalent (DE) due to photoneutrons in tissue (17-21). and some of them (18, 22) calculated the DE of fast neutrons in voxel-based phantoms. Calculating the effects of each category of photoneutrons along the beam axis, in water equivalent and water phantoms were conducted by many other researchers (4, 5, 23-28).

According to published researches, different materials and thickness of target have influence on dose rate and production of photoneutrons (29-32). Geo et al. (29) studied the effects of thickness of several materials on dose rate and leakage of electron for 6 MeV electron beam.

Berger and Seltzer (30) described calculations of bremsstrahlung production and associated photoneutron production in thick targets irradiated by electron beams with energies between 10 and 60 MeV. They showed that the target plays an important role in the production of photon and yield of photoneutron.

It is shown that the main components which produce contaminant photoneutrons are primary collimator, secondary collimator and target (33, 34). Manipulation of target for reducing the photoneutron yield of a linac is more applicable and easier rather than collimators. Commonly the target of linacs is made of tungsten. In a study, Rojas-Arias et al. (31) proposed a new self-made alloy ($\text{Ti}_2\text{V}_{0.7}\text{Cu}_{97.3}$) as the target of linac. They showed when a plate of this alloy was irradiated with a 16 MeV beam of electrons, smaller number of photoneutrons produce in comparison with tungsten plate. In this research we intend to calculate the proportion of photoneutron fluence, kerma and dose equivalent of photoneutrons in axial and transverse directions within an ICRU phantom using MCNPX simulation code for the proposed target [by Rojas-

Arias et al. (31)] in 18 MV Varian linac 2100 C/D machine (hereafter new machine) and compare them with conventional machine with tungsten target (hereafter current machine). To consider the role of nitrogen and similarity to the tissue of the body, we used ICRU soft tissue equivalent phantom in simulations. Most of the researchers have studied photoneutrons distributions in the air of the treatment room and only few works studied photoneutrons within soft tissue equivalent phantom.

Materials and Methods

A typical treatment room (28) with walls, ceiling (thickness of 1.7 m) and floor (thickness of 1 m) from concrete simulated. For calculating the required quantities, the MCNPX Monte Carlo code, Version 2.6, was applied. Current and new machines are the same except the material of the target. The head of the linac including all effective components therein containing target (tungsten for current machine and $\text{Ti}_2\text{V}_{0.07}\text{Cu}_{97.93}$ for new machine), primary collimator (W), vacuum window (Be), flattening filter (Fe and Ta), ionization chamber (Cu and Kapton), secondary collimator (W and Pb), mirror (Mylar), Jaws (W), and upper circle (Fe) were simulated. The energy of linacs was 18 MeV in photon mode. The fluence, dose equivalent and kerma of photoneutrons calculated at 105 points, at axial and transvers directions of incident photon beam, within an ICRU soft tissue phantom. Field size of the treatment photon beam was $10 \times 10 \text{ cm}^2$ and SSD= 100 cm. More details are in previous work (10).

F4 tally is for calculating transmitted flux of the particle in terms of number of particles per square centimeter (n.cm^{-2}), which could be converted to DE using Flux-to-Dose Rate Conversion factor and Quality Factor in terms of mSv/Gy-X (Appendix H of MCNPX user's manual). The values of these factors are related to

energy of photons, and have specific amount for every range of energy. Energy ranges and conversion factors were entered to input file using "dose energy" and "dose function" cards, respectively. In this research, for this purpose, NCRP NO. 38 recommended factors were used. Kerma acquired by means of F6 tally in terms of $\text{MeV.g}^{-1}/\text{electron}$, which was changed to mGy.Gy^{-1} .

Results

At first, neutron source strength was calculated for new machine based on McGinley and Landry method (9). The result was $0.85 \times 10^{12} \text{ n/Gy}$ in comparison with $1.37 \times 10^{12} \text{ n/Gy}$ for current machine. These outputs obviously showed that production of photoneutrons has decreased for new machine.

The fluence, kerma, and dose equivalent of photoneutrons along the central axis at 34 points of ICRU phantom from the depth of 0.1 cm to 29 cm for current and new machine are depicted in Figure 1.

The fluence, kerma, and dose equivalent of total photoneutrons along the transvers direction at 80 points at depths of 0.1, 1, 10 and 20 cm of the ICRU phantom were shown in Figures 2-4.

Discussion

Since the elements in new alloy have lower atomic number than tungsten, it is expected that production of photoneutrons be less than tungsten, too. Calculations demonstrated this fact; the neutron source strength for new machine is 68 % of common machine.

Figure 1a shows that the amounts of fluence, kerma and dose equivalent at all points are less for new machine. These quantities decrease rapidly to depth of 15 cm (i.e., for fluence after depth of 2 cm) and then the curves become nearly constant, which is in accordance with Kry's findings (19), for tungsten target.

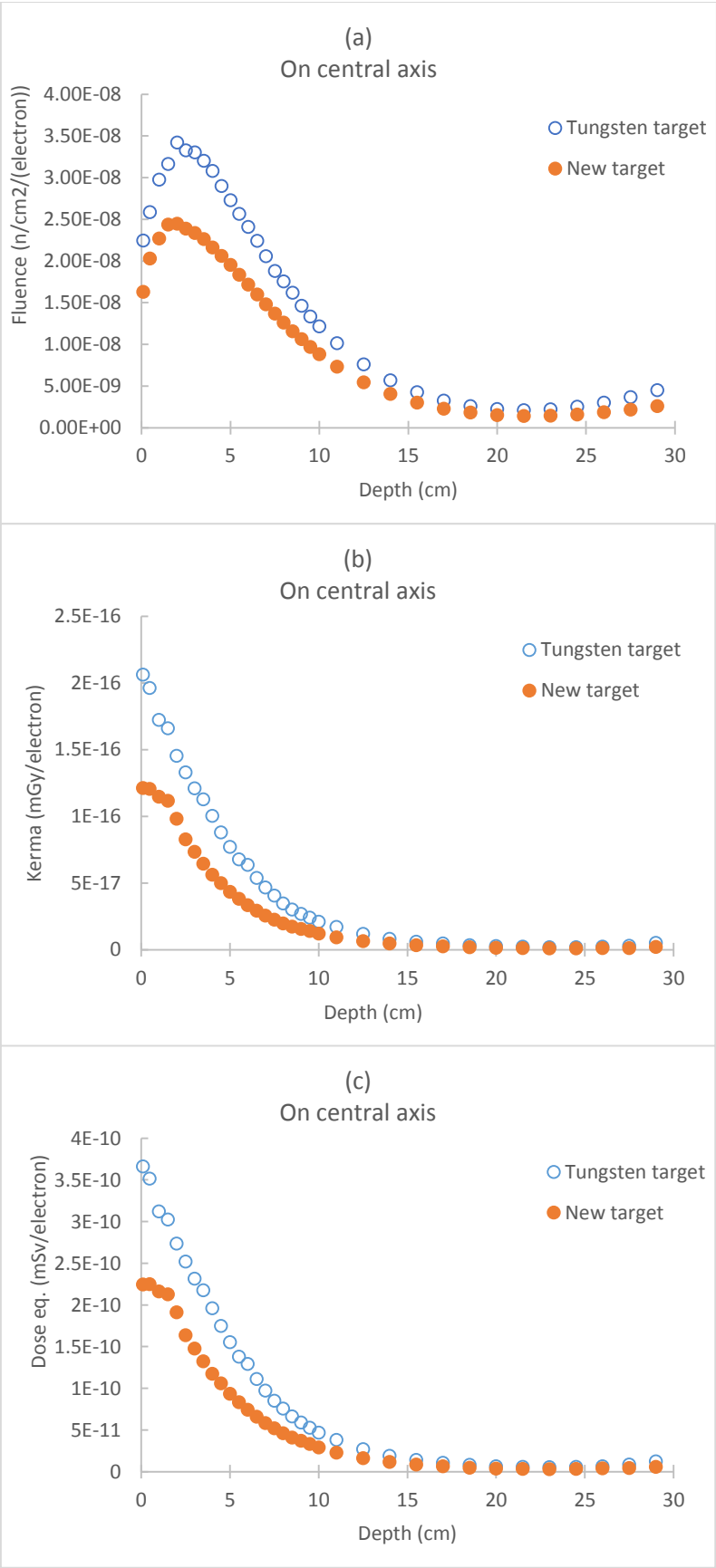


Figure 1. The (a) fluence, (b) kerma, and (c) dose equivalent of photoneutrons along the central axis of ICRU phantom for current and new machine.

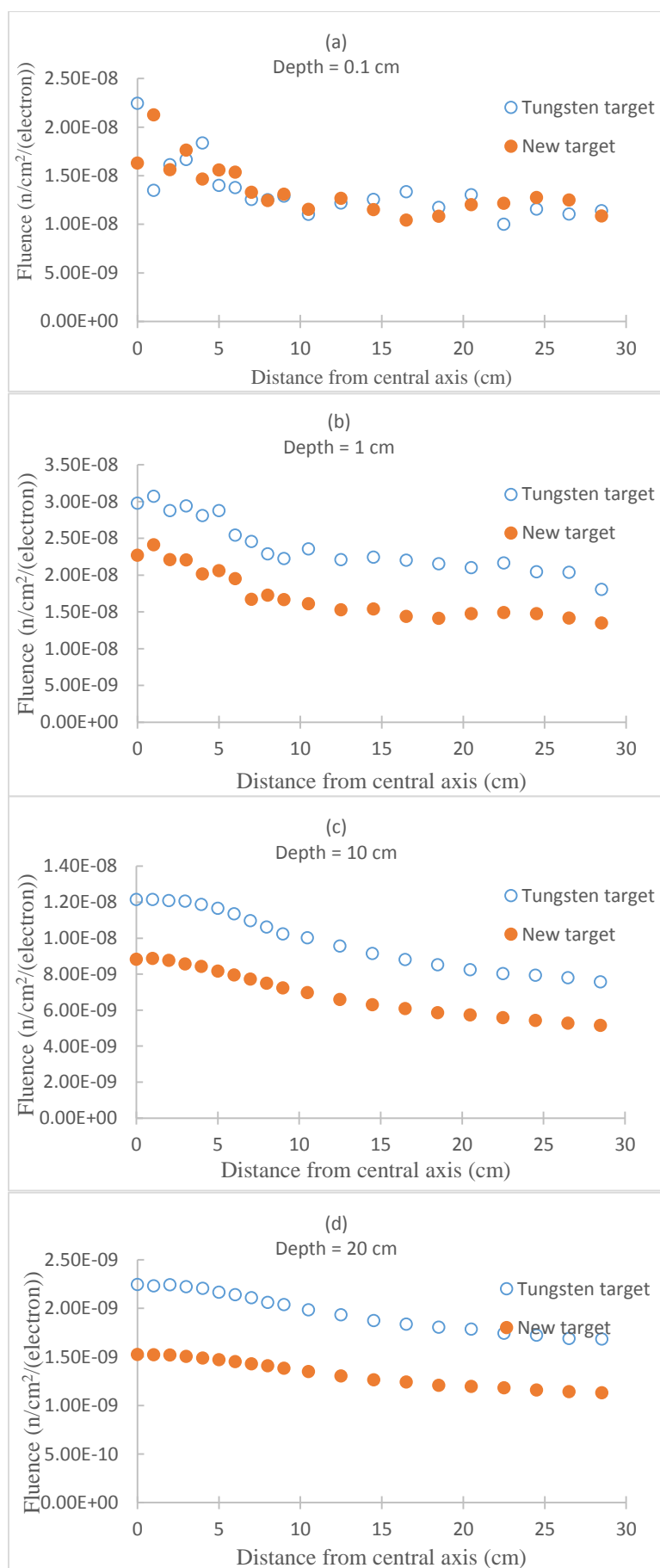


Figure 2. Fluence of photoneutrons at lateral direction in depths (a) 0.1 cm, (b) 1 cm, (c) 10 cm and (d) 20 cm.

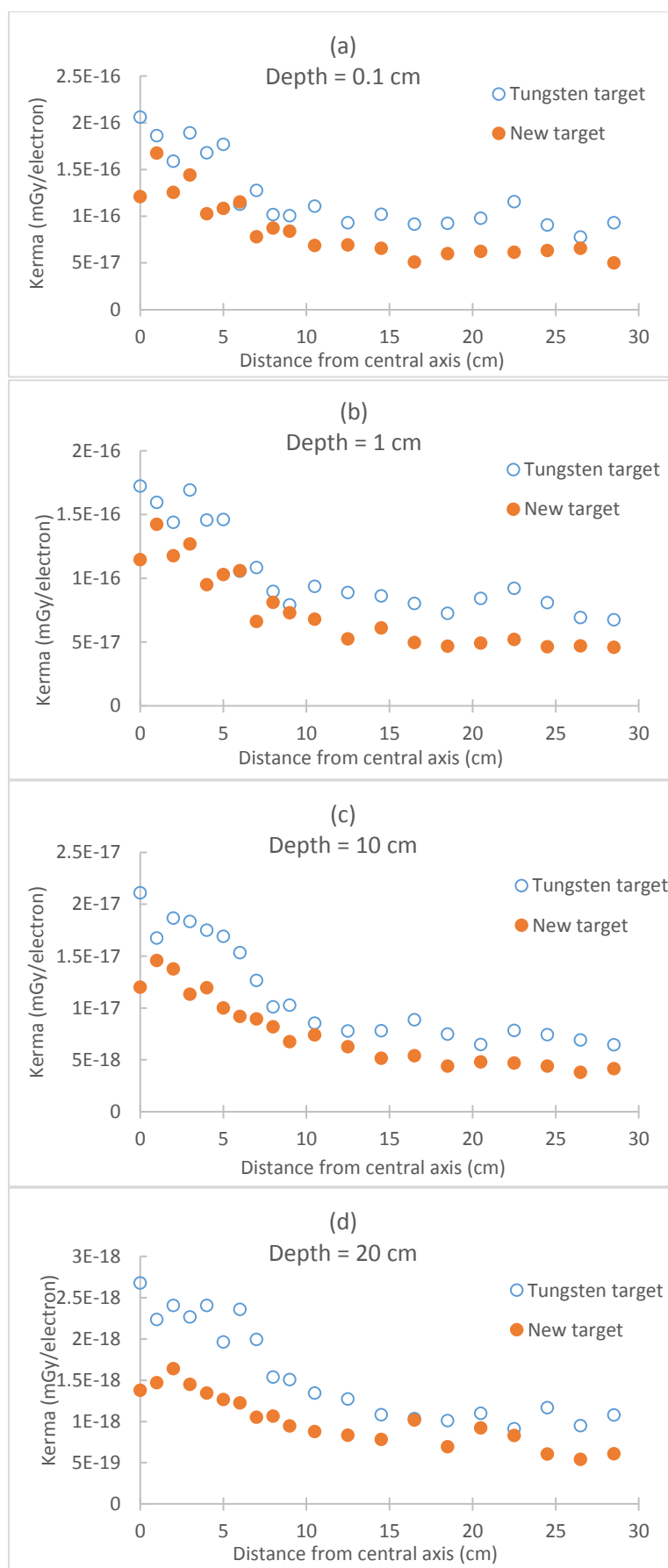


Figure 3. Kerma of photoneutrons at lateral direction in depths (a) 0.1 cm, (b) 1 cm, (c) 10 cm and (d) 20 cm.

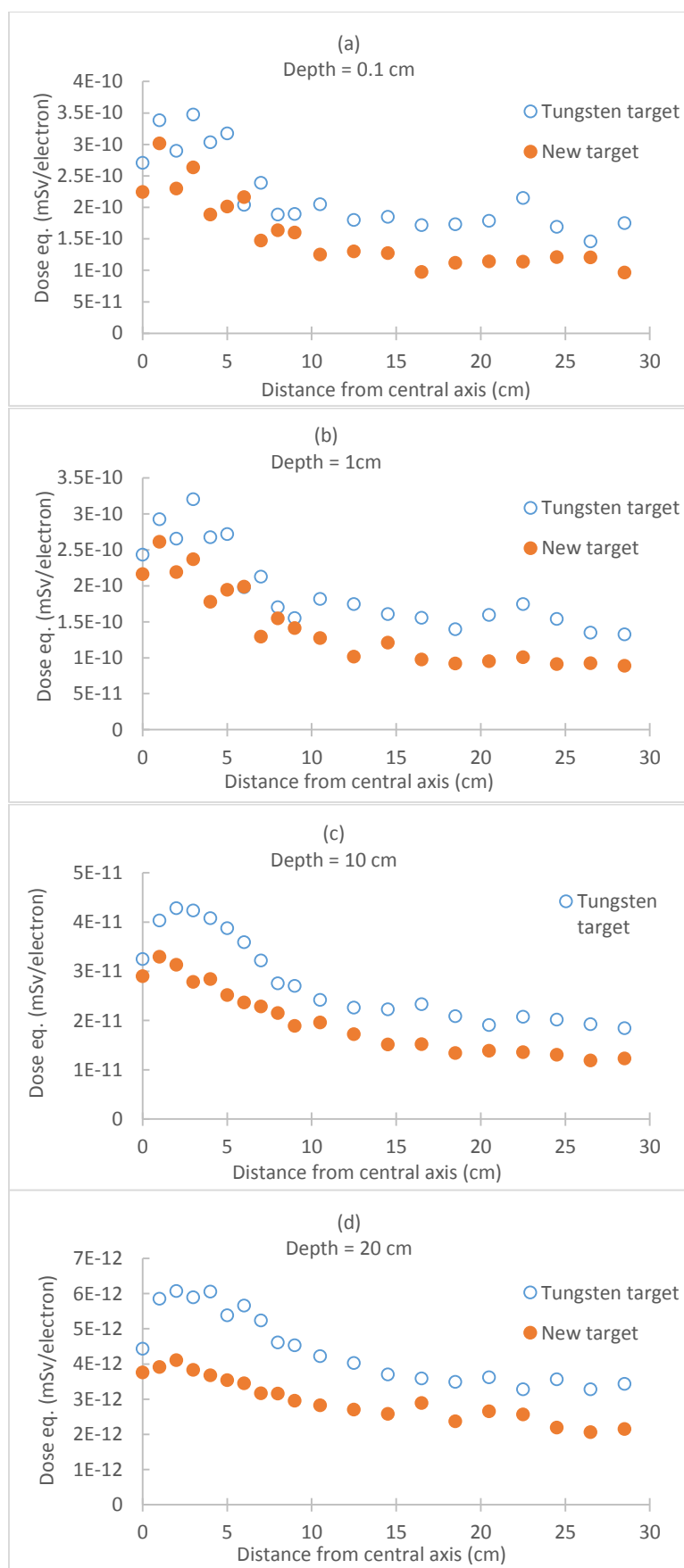


Figure 4. Dose equivalent of photoneutrons at lateral direction in depths (a) 0.1 cm, (b) 1 cm, (c) 10 cm and (d) 20 cm.

For comparing the results quantitatively, the phantom was divided into two areas: depths less than 15 cm (*shallow area*) and depths more than 15 cm (*deep area*).

Ratios of maximums of fluence, kerma, and dose equivalent at axial direction in machine with new target to machine with tungsten target are 0.72, 0.59, and 0.61, respectively. Ratio of these quantities in average at shallow and deep areas are 0.72, 0.60, 0.56; and 0.65, 0.50, 0.64, respectively. All over, these findings show all three quantities at axial directions are less in machine with new target.

Figure 2 shows the fluence of photoneutrons at lateral direction at 0.1, 1, 10 and 20 cm depths. These diagrams show that at distances less than 5 cm and distances more than 10 cm the curves are almost horizontal and at distances between 5 and 10 cm they are descending. Because the field size was $10 \times 10 \text{ cm}^2$, so the edge of incident photon beam is at 5 cm from central axis and the number of photoneutrons is more in the photon field. So, we can divide the phantom laterally into three areas: *inner area* (distances less than 5 cm from central axis), *penumbra area* (distances between 5 and 10 cm) and *outer area* (distances more than 10 cm). This manner is on expectation, because it was shown that fluence of photoneutrons is higher within the photon field (35,18).

Figures 3 and 4 shows the kerma and dose equivalent of photoneutrons at lateral direction in depths 0.1, 1, 10 and 20 cm, respectively. Kry and et al., (19) using MCNPX code have derived a curve for dose equivalent only for surface of the phantom, in the same conditions for tungsten target, and our result (dose equivalent at depth 0.1 cm) is very close to these amounts which in another paper (10) depicted and compared these two diagrams. Ratios of fluence in average at lateral directions (i.e., at 0.1, 1, 10 and 20 cm depths) in machine with new target to machine with tungsten target at inner area (i.e., axial distances less than 5 cm) and outer area (i.e., axial distances more than 5

cm) are 0.78, and 0.74, respectively. Ratios of kerma and dose equivalent in average for new target and tungsten target at inner area and outer area are 0.70, 0.65; and 0.75, 0.66, respectively. Overall, these findings show that the fluence, kerma and dose equivalent in lateral directions are less in machine with new target.

Conclusion

Along central axis of the treatment beam, in the ICRU soft tissue phantom, the fluence, kerma, and dose equivalent of produced unwanted photoneutrons for the linac which its target is made of new alloy ($\text{Ti}_2\text{V}_{0.7}\text{Cu}_{97.3}$) are less than the linac with tungsten target.

Calculation of photoneutron production in both central axis and transverse directions within the ICRU phantom showed that photoneutron fluence, kerma and dose equivalent decreased remarkably by applying the new target in the linac and verify that this introduced alloy is suitable for setting in the head of linacs. Though this alloy mainly composed of copper, but heat removal of copper ($401 \text{ W/m}^2\text{.}^\circ\text{C}$) is larger in comparison with tungsten ($174 \text{ W/m}^2\text{.}^\circ\text{C}$) (31).

In future works one can calculate the photon yield as well as electron contamination of this new target, to gain more knowledge of this new machine. Authors suggest another research by applying some neutron absorbers as protective aprons during treatment and calculating or measuring the photoneutron contamination in presence of these protective materials.

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Conflict of Interest

There is no conflict of interest regarding this research.

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